Exact solution for a Stefan problem with convective boundary condition and density jump

Domingo A. Tarzia*

CONICET - Depto. Matemática, FCE, Univ. Austral, Paraguay 1950, S2000FZF Rosario, Argentina.

We consider the solidification of a semi-infinite material which is initially at its liquid phase at a uniform temperature T_i . Suddenly at time t>0 the fixed face x=0 is submitted to a convective cooling condition with a time-dependent heat transfer coefficient of the type $H(t)=ht^{-1/2}$ (h>0) The bulk temperature of the liquid at a large distance from the solid-liquid interface is T_{∞} , a constant temperature such that $T_{\infty} < T_f < T_i$ where T_f is the freezing temperature. We also consider the density jump between the two phases. We obtain that the corresponding phase-change (solidification) process has an explicit solution of a similarity type for the temperature of both phases and the solid-liquid interface, if and only if the coefficient h is large enough, that is $h>h_0=\frac{k_l}{\sqrt{\pi \alpha_l}}\frac{T_l-T_f}{T_l-T_{\infty}}$ where k_l and α_l are the conductivity and diffusion coefficients of the initial liquid phase. Moreover, when $h\leq h_0$ we only have a heat conduction problem for the initial liquid phase and the corresponding change of phase does not occur. We do the mathematical analysis of a problem which was presented in S.M. Zubair - M.A. Chaudhry, Wärme-und-Stoffübertragung, 30 (1994), 77-81 and we generalized the results obtained in D.A. Tarzia, MAT-Serie A, 8 (2004), 21-27 when the density jump between the two phases was neglected.

© 2007 WILEY-VCH Verlag GmbH & Co. KGaA, Weinheim

1 Introduction

Heat transfer problems involving a change of phase due to melting or freezing processes are very important in science and technology [3], [5]. This kind of problems are generally refered as moving-free boundary problems which have been the subject of numerous theoretical, numerical and experimental investigations, e.g. we can see the large bibliography on the subject given in [7]. We consider the solidification of a semi-infinite material which is initially at its liquid phase at a uniform temperature T_i . Suddenly at time t>0 the fixed face x=0 is submitted to a convective cooling condition due to a sudden drop in the ambient temperature. The bulk temperature of the liquid at a large distance from the solid-liquid interface is T_{∞} , a constant such that $T_{\infty} < T_f < T_i$ where T_f is the freezing temperature. The density jump between the two phases are also considered. In order to solve the phase-change process with a convective condition at the fixed face x=0, approximate method were used, for example in [1], [2], [4]. In [9] the problem was analyzed and a closed-form expression for the solid-liquid interface and both temperatures were found when the heat transfer coefficient h is time-dependent and proportional to $t^{-\frac{1}{2}}$. The solution is obtain graphically. The goal of this paper is to give the mathematical analysis of this problem, that is the solidification of a semi-infinite material which is initially at the constant temperature T_i and a convective cooling condition is impossed at the fixed boundary x=0 for a time-dependent heat transfer coefficient of the type

$$H(t) = h/\sqrt{t}, \ h > 0, \ t > 0,$$
 (1)

and the density jump between the two solid and liquid phases are also considered. We prove that there exists an instantaneous phase-change process if and only if the coefficient h is large enough, that is

$$h > \frac{k_l}{\sqrt{\pi \alpha_l}} \frac{T_i - T_f}{T_i}$$
where k_i and $\alpha_i = k_i/\rho_i c_i$ are the conductivity and diffusion coefficients of the phase i ; c_i and ρ_i are the specific heat and the mass density of the phase i ($i = c_i$ solid) $i = l$; liquid). Moreover, the applicit approximation for the phase i ($i = c_i$ solid) $i = l$; liquid). Moreover, the applicit approximation for the phase i ($i = c_i$ solid) $i = l$; liquid).

where k_i and $\alpha_i = k_i/\rho_i c_i$ are the conductivity and diffusion coefficients of the phase i; c_i and ρ_i are the specific heat and the mass density of the phase i (i = s: solid; i = l: liquid). Moreover, the explicit expression for the solid-liquid interface s (t) and the temperatures of the solid T_s (x, t) and liquid T_l (x, t) phases respectively can be obtained if and only if the inequality (2) is verified for the coefficient h which characterizes the dependent-time heat transfer coefficient H (t) given by (1).

2 Explicit solution for a convective boundary condition and density jump.

We consider the following free boundary problem: find the solid-liquid interface x=s(t) and the temperature T(x,t) defined by $T_s(x,t)$ if 0 < x < s(t), t > 0, T_f if x=s(t), t > 0 and $T_l(x,t)$ if x > s(t), t > 0 which satisfy the following equations and boundary conditions

$$T_{s_t} = \alpha_s T_{s_{xx}}, \ 0 < x < s(t), \ t > 0 \tag{3}$$

^{*} e-mail: Domingo.Tarzia@fce.austral.edu.ar, Phone: +54 341 5223093, Fax: +54 341 5223001

$$T_{l_t} \bigoplus \frac{\rho_s - \rho_l}{\rho_l} \dot{s}(t) T_{l_x} = \alpha_l T_{l_{xx}}, \ x > s(t), \ t > 0$$

$$\tag{4}$$

$$T_s(s(t),t) = T_t(s(t),t) = T_f, \ x = s(t), \ t > 0$$
 (5)

$$T_l(x,0) = T_l(+\infty,t) = T_i, \ x > 0, \ t > 0$$
 (6)

$$k_s T_{s_x}(0,t) = \frac{h}{\sqrt{t}} \left(T_s(0,t) - T_{\infty} \right), \ t > 0$$
 (7)

$$k_s T_{s_x}(s(t), t) - k_l T_{l_x}(s(t), t) = \rho_s l \dot{s}(t), t > 0$$
 (8)

$$s(0) = 0 \tag{9}$$

where l is the latent heat of fusion, and $T_{\infty} < T_f < T_i$.

We obtain the following results:

Theorem 2.1 (i) If the coefficient h verifies the inequality (2) then the free boundary problem (3)—(9) has the explicit solution of a similarity type given by

$$s(t) = 2\xi\sqrt{\alpha_s t} \tag{10}$$

$$T_{s}\left(x,t\right) = T_{\infty} + \frac{\left(T_{f} - T_{\infty}\right)\left[1 + \frac{h\sqrt{\pi\alpha_{s}}}{k_{s}}\operatorname{erf}\left(\frac{x}{2\sqrt{\alpha_{s}t}}\right)\right]}{1 + \frac{h\sqrt{\pi\alpha_{s}}}{k_{s}}\operatorname{erf}\left(\xi\right)}, \quad 0 < x < s\left(t\right), \quad t > 0$$

$$\text{(11)}$$

$$T_{l}(x,t) = T_{f} + (T_{i} - T_{f}) \left[erf \left(\delta + \frac{x}{2\sqrt{\alpha_{l}t}} \right) - erf \left((1+\varepsilon)\sqrt{\frac{\alpha_{s}}{\alpha_{l}}}\xi \right) \right], \quad x > s(t), \quad t > 0$$

$$(12)$$

where erf is the error function and erfc is the complementary error function defined by $\operatorname{erfc}(z) = 1 - \operatorname{erf}(z)$, and the dimensionless parameter $\xi > 0$ satisfies the following equation

$$G\left(x\right) = x, \ x > 0 \tag{13}$$

where function G and the coefficients δ and ε are given by

$$G(x) = b_1 \frac{\exp\left(-x^2\right)}{1 + b_2 \operatorname{erf}(x)} - b_3 \frac{\exp\left(-b^2 x^2\right)}{\operatorname{erfc}(bx)}$$

$$\tag{14}$$

$$\delta = \varepsilon \xi \sqrt{\frac{\alpha_s}{\alpha_l}}, \quad \varepsilon = \frac{|\rho_s - \rho_l|}{\rho_l}, \quad \alpha_0 = \frac{\alpha_l}{(1 + \varepsilon)^2}, \quad b = \sqrt{\frac{\alpha_s}{\alpha_0}}, \tag{15}$$

$$b_1 = \frac{h(T_f - T_\infty)}{\rho_s l\sqrt{\alpha_l}}, \qquad b_2 = b_1 \frac{h}{k_s} \sqrt{\pi \alpha_s}; \qquad b_3 = \frac{k_l(T_i - T_f)}{\rho_s l\sqrt{\alpha_s \alpha_l \pi}}.$$
 (16)

(ii) The Eq. (13) has a unique solution ξ if and only if the coefficient h satisfies the inequality (2). In this case, there exists an instantaneous solidification process.

Remark 2.2 (i) We note that the temperature at the fixed face x = 0 is given by $T_s(0,t) = Const. < T_f$.

- (ii) We note that the inequality (2) for the coefficient h is of the type that it was obtained in [6] when a time-dependent heat flux condition on the fixed face is impossed.
 - (iii) When the jump density between the two phases is negleted, i.e. $\varepsilon = 0$, then we find the result obtained in [8].

Acknowledgements This paper has been partially sponsored by the projects PIP#5379 from CONICET-UA, Rosario (Argentina), AN-PCYT PAV #120-00005 from Agencia (Argentina) and Fondo de ayuda a la Investigación de la Univ. Austral (Argentina).

References

- [1] P.M. Beckett "A note on surface heat transfer coefficients", Int. J. Heat Mass Transfer, 34, 2165-2166 (1991).
- [2] S.D. Foss, "An approximate solution to the moving boundary problem associated with the freezing and melting of lake ice", A.I.Ch.E. Symposium Series, 74, 250-255 (1978).

- Symposium Series, 74, 230-233 (1976).

 [3] S.C. Gupta, "The classical Stefan problem. Basic concepts, modeling and analysis", Elsevier, Amsterdam (2003).

 [4] T.J. Lu, "Thermal management of high power electronic with phase change cooling", Int. J. Heat Mass Transfer, 43, 2245-2256 (2000).

 [5] V.J. Lunardini "Heat transfer with freezing and thawing", Elsevier, Amsterdam (1991).

 [6] D.A. Tarzia, "An inequality for the coefficient σ of the free boundary $s(t) = 2\sigma\sqrt{t}$ of the Neumann solution for the two-phase Stefan
- problem", Quart. Appl. Math, 39, 491-497 (1981-82).

 [7] D.A. Tarzia, "A bibliography on moving free boundary problems for the heat-diffusion equation. The Stefan and related problems",
- MAT-Serie A, #2 (2000) (with 5869 titles on the subject, 300 pages). See www.austral.edu.ar/MAT-SerieA/2(2000).
 [8] D.A. Tarzia, "An explicit solution for a two-phase unidimensional Stefan problem with a convective boundary condition at the fixed face", MAT-Serie A, #8, 21-27 (2004).
- [9] S.M. Zubair and M.A. Chaudhry "Exact solutions of solid-liquid phase-change heat transfer when subjected to convective boundary conditions", Wärme- und Stoffübertragung (now Heat and Mass Transfer), 30, 77-81 (1994).