

An inequality for the constant heat flux to obtain a steady-state two-phase Stefan problem

DOMINGO A. TARZIA

Promar (Conicet-U.N.R.), Instituto de Matemática 'Beppo Levi', Facultad de Ciencias Exactas e Ing., Av. Pellegrini 250, (2000) Rosario, Argentina

We consider a material $\Omega \subset \mathcal{R}^n$ with regular boundary $\Gamma = \Gamma_1 \cup \Gamma_2$ and we assume that the melting temperature is 0°C . We apply a temperature $b > 0$ on Γ_1 and a heat flux $q > 0$ on Γ_2 . We prove that there exists a constant $q_1 > 0$ such that, for $q > q_1$, we have a steady-state two-phase Stefan problem. This result is verified numerically, by using Modulef, with two cases with analytical solutions.

1. INTRODUCTION

We consider a material Ω , a bounded domain of \mathcal{R}^n ($n = 1, 2, 3$ for the applications), with a sufficiently regular boundary $\Gamma = \Gamma_1 \cup \Gamma_2$ (with measure $(\Gamma_1) > 0$) and we assume that the phase-change temperature is 0°C . We apply a constant temperature $b > 0$ on Γ_1 and a constant (outcoming) heat flux $q > 0$ on Γ_2 . If we consider in Ω a steady-state heat conduction problem, from the physical point of view, we arrive at the following conclusions:

- (i) If q is small, then the temperature in Ω will be positive, and so a change of phase in the material will not occur. In this case, the resulting problem will be one of conduction, only for the liquid phase.
- (ii) If q is large, then the temperature in Ω will take positive and negative values, and so a change of phase in the material will occur.

In this paper, we shall find for q a sufficient condition for the occurrence of a change of phase in Ω , i.e., we shall prove that there exists $q_1 > 0$ so that for all $q > q_1$ we can have a steady-state two-phase Stefan problem in Ω . Moreover, in two examples where the sufficient conditions is also necessary¹, we shall compute numerically the constant q_1 through a simulation process by using the Modulef software (Finite Elements Modules).

2. MATHEMATICAL FORMULATION OF THE PROBLEM

Following² we study the temperature $\theta = \theta(x)$, defined for $x \in \Omega$. The set Ω can be expressed in this form

$$\Omega = \Omega_1 \cup \Omega_2 \cup L \quad (1)$$

where

$$\begin{aligned} \Omega_1 &= \{x \in \Omega / \theta(x) < 0\} & \Omega_2 &= \{x \in \Omega / \theta(x) > 0\} \\ L &= \{x \in \Omega / \theta(x) = 0\} \end{aligned} \quad (2)$$

are the solid phase, the liquid phase and the free boundary that separates them respectively.

The temperature θ can be represented in Ω in the following way:

$$\theta(x) = \begin{cases} \theta_1(x) < 0 & x \in \Omega_1 \\ 0 & x \in L \\ \theta_2(x) > 0 & x \in \Omega_2 \end{cases} \quad (3)$$

and satisfies the following conditions

$$\begin{aligned} \Delta \theta_i &= 0 & \text{in } \Omega_i \ (i=1, 2) \\ \theta_1 &= \theta_2 = 0 & k_1 \frac{\partial \theta_1}{\partial n} = k_2 \frac{\partial \theta_2}{\partial n} \text{ on } L \end{aligned} \quad (4)$$

$$\begin{aligned} \theta_2 / \Gamma_1 &= b \\ -k_2 \frac{\partial \theta_2}{\partial n} \Big|_{\Gamma_2} &= q \quad \text{si } \theta / \Gamma_2 > 0 \\ -k_1 \frac{\partial \theta_1}{\partial n} \Big|_{\Gamma_2} &= q \quad \text{si } \theta / \Gamma_2 < 0 \end{aligned}$$

where $k_i > 0$ is the thermal conductivity of phase i ($i=1$: solid phase, $i=2$: liquid phase), $b > 0$ is the constant temperature given on Γ_1 , and $q > 0$ is the constant heat flux given on Γ_2 .

If we define the function u in Ω as follows

$$u = k_2 \theta^+ - k_1 \theta^- \quad \text{in } \Omega \quad (5)$$

where θ^+ and θ^- represent the positive part and the negative part of the function θ respectively, then problem (4) is transformed into

$$\begin{aligned} \Delta u &= 0 & \text{in } D'(\Omega) \\ u / \Gamma_1 &= b_0 \equiv k_2 b \\ -\frac{\partial u}{\partial n} \Big|_{\Gamma_2} &= q \end{aligned} \quad (6)$$

Accepted May 1988. Discussion closes May 1989

whose variational formulation is given by

$$\begin{aligned} a(u, v-u) &= -q \int_{\Gamma_2} (v-u) d\gamma \quad v \in K \\ u &\in K \end{aligned} \quad (7)$$

where

$$\begin{aligned} V &= H^1(\Omega) \quad V_0 = \{v \in V / v|_{\Gamma_1} = 0\} \\ K &= \{v \in V / v|_{\Gamma_1} = b_0\} \\ a(u, v) &= \int_{\Omega} \nabla u \cdot \nabla v dx \end{aligned} \quad (8)$$

Moreover, the solution of (7) is characterized by the following minimum problem³⁻⁵:

$$\begin{cases} J(u) \leq J(v) & v \in K \\ u \in K \end{cases} \quad (9)$$

where

$$J(v) = \frac{1}{2} a(v, v) + q \int_{\Gamma_2} v d\gamma \quad (10)$$

Remark 1

The inverse transformation of (5) is given by

$$\theta = \frac{1}{k_2} u^+ - \frac{1}{k_1} u^- \quad \text{in } \Omega \quad (5 \text{ bis})$$

3. PROPERTIES

Let u_q be the unique solution of the variational equation (7) for $q > 0$ (Ref. 2).

Property 1

We have the following expression

$$a(u_q^-, u_q^-) = q \int_{\Gamma_2} u_q^- d\gamma \quad (11)$$

Proof. It is enough to choose $v = u_q^+ \in K$ in (7) to obtain (11).

Remark 2

From (11) and from the fact that $u_q^- \in V_0$, we deduce the equivalence

$$u_q^- \not\equiv 0 \text{ en } \Omega \Leftrightarrow u_q^- \not\equiv 0 \text{ sobre } \Gamma_2 \quad (12)$$

from which, for a given value of q , we have that there will be a change of phase in Ω (u_q or θ_q take positive and negative values in Ω) iff the function u_q takes negative values on the boundary Γ_2 . In other words, the function u_q will begin to take negative values on Γ_2 . (This fact will be taken into account when we carry out the numerical simulation for the computation of the coefficient q_1 .)

Property 2

If $u_i \equiv u_{q_i}$ is the solution of (7) for q_i ($i = 1, 2$), then we have the following equalities:

$$\begin{aligned} \text{(i)} \quad a(u_2 - u_1, u_2 - u_1) &= (q_1 - q_2) \int_{\Gamma_2} (u_2 - u_1) d\gamma \\ \text{(ii)} \quad a(u_2, u_2) - a(u_1, u_1) &= a(u_2 + u_1, u_2 - u_1) \\ &= (q_1 + q_2) \int_{\Gamma_2} (u_1 - u_2) d\gamma \end{aligned} \quad (13)$$

Proof. If we take $v = u_2 \in K$ in the variational equality corresponding to u_1 , and $v = u_1 \in K$ in the one corresponding to u_2 and we add up and subtract both equalities, then we obtain (13i) and (13ii) respectively.

Property 3

If $u_i = u_{q_i}$ is the unique solution of (7) for q_i ($i = 1, 2$), then we have the following properties:

(i) If $q_2 \leq q_1$ then

$$\text{(a)} \quad u_1 \leq u_2 \quad \text{in } \Omega \quad \text{(b)} \quad \int_{\Gamma_2} u_1 d\gamma \leq \int_{\Gamma_2} u_2 d\gamma \quad (14)$$

(ii) The applications $q \rightarrow u_q$ and $q \rightarrow \int_{\Gamma_2} u_q d\gamma$ are strictly decreasing functions. i.e.,

$$\begin{aligned} \text{(a)} \quad u_1 \leq u_2, u_1 \neq u_2 \quad \text{in } \Omega \\ q_2 < q_1 \Rightarrow \text{(b)} \quad \int_{\Gamma_2} u_1 d\gamma < \int_{\Gamma_2} u_2 d\gamma \end{aligned} \quad (15)$$

Proof. (i) Condition (14b) follows directly from (13i). To prove (14a) we shall take into account the following equivalence:

$$\begin{cases} u_1 \leq u_2 \quad \text{in } \Omega \Leftrightarrow W = 0 \quad \text{in } \Omega \\ \text{where } W = (u_2 - u_1)^- \end{cases} \quad (16)$$

Since $W \in V_0$, then, if we use $v = u_2 + W \in K$ in the variational equality corresponding to u_1 , and $v = u_1 + W \in K$ in the one corresponding to u_2 and we later add them up, we have

$$0 \leq (q_1 - q_2) \int_{\Gamma_2} W d\gamma = a(u_2 - u_1, W) = -a(W, W) \leq 0 \quad (17)$$

that is, $W = 0$ in Ω .

(ii) To prove (15a,b) we use the following results:

$$\text{(A)} \quad u_1 = u_2 \quad \text{in } \Omega \Rightarrow q_1 = q_2 \quad \text{or} \quad \int_{\Gamma_2} (u_2 - u_1) d\gamma = 0 \quad (18)$$

$$\text{(B)} \quad \int_{\Gamma_2} (u_2 - u_1) d\gamma = 0 \Rightarrow \begin{cases} \text{(Bi)} & u_2 = u_1 \quad \text{in } \Omega \\ \text{(Bii)} & q_1 = q_2 \end{cases} \quad (19)$$

Condition (A) results directly from (13i) and condition (Bi) is deduced from (13i) and from the fact that $u_2 - u_1 \in V_0$. Taking into account (B)'s hypothesis, the result (Bi) and the variational equalities corresponding to u_2 and u_1 , we obtain

$$\begin{aligned}
 -q_1 \int_{\Gamma_2} (v-u_1) d\gamma &= a(u_1, v-u_1) = a(u_2, v-u_2) \\
 &= -q_2 \int_{\Gamma_2} (v-u_2) d\gamma = -q_2 \int_{\Gamma_2} (v-u_1) d\gamma \quad v \in K
 \end{aligned}$$

i.e.,

$$(q_1 - q_2) \int_{\Gamma_2} (v-u_1) d\gamma = 0 \quad v \in K \quad (20)$$

Taking one element $v_0 \in V_0$ so that $\int_{\Gamma_2} v_0 d\gamma \neq 0$ and choosing $v = u_1 + v_0 \in K$, from (20) we deduce (Bii).

Let $f: \mathbb{R}^+ \rightarrow \mathbb{R}$ be the real function, defined in the following way:

$$f(q) = J(u_q) = \frac{1}{2} a(u_q, u_q) + q \int_{\Gamma_2} u_q d\gamma \quad (21)$$

Remark 3

To find the element q_1 (see Introduction), and taking into account (12), (15b) and function f , it will be enough to find a value $q > 0$ for which we have $f(q) < 0$. We shall further see that this technique can still be improved.

Property 4

For all $q > 0$ and h such that $q+h > 0$, we have the following estimations:

$$(i) \left\| \frac{1}{h} (u_{q+h} - u_q) \right\|_V \leq C_1 \equiv \frac{\|\gamma_0\|}{\alpha_0} [\text{meas}(\Gamma_2)]^{1/2} \quad (22)$$

$$(ii) \left\| \frac{1}{h} (u_q - u_{q+h}) \right\|_{L^2(\Gamma_2)} \leq C_2 \equiv C_1 \|\gamma_0\| \quad (23)$$

where γ_0 is the trace operator (linear and continuous, defined on V), and $\alpha_0 > 0$ is the coercivity constant on V_0 of the bilinear form a , i.e.,

$$a(v, v) \geq \alpha_0 \|v\|_V^2 \quad v \in V_0 \quad (24)$$

Proof. (i) Taking into account (24), (13i) with $q_1 = q+h$ and $q_2 = q$, the Cauchy-Schwarz inequality and the continuity of γ_0 we obtain (22). (ii) Taking into account (22) and the continuity of γ_0 , we deduce (23).

From (15b) and (23) we deduce the following

Corollary 5

From all $q > 0$ and $h > 0$ we have

$$0 < \int_{\Gamma_2} u_q d\gamma - \int_{\Gamma_2} u_{q+h} d\gamma < C_2 h \quad (25)$$

and therefore the function $q \rightarrow \int_{\Gamma_2} u_q d\gamma$ is continuous.

Property 6

Function f is derivable. Moreover, f' is continuous and strictly decreasing function, and it is given by the following expression

$$f'(q) = \int_{\Gamma_2} u_q d\gamma \quad (26)$$

Proof. From (13ii) we obtain

$$\frac{f(q+h) - f(q)}{h} = \frac{1}{2} \int_{\Gamma_2} u_q d\gamma + \frac{1}{2} \int_{\Gamma_2} u_{q+h} d\gamma \quad (27)$$

and the expression (26) is deduced from (25) and (27).

Property 7

For all $q > 0$ we have the following expressions

$$(i) a(u_q, u_q) = k_2 b \int_{\Gamma_1} \frac{\partial u_q}{\partial n} d\gamma - q \int_{\Gamma_2} u_q d\gamma \quad (28)$$

$$(ii) \int_{\Gamma_1} \frac{\partial u_q}{\partial n} d\gamma = q \text{meas}(\Gamma_2) \quad (29)$$

$$(iii) f(q) = k_2 b \text{meas}(\Gamma_2) q - \frac{1}{2} a(u_q, u_q) \quad (30)$$

$$(iv) \frac{d}{dq} [a(u_q, u_q)] = 2 \left[k_2 b \text{meas}(\Gamma_2) - \int_{\Gamma_2} u_q d\gamma \right] = \frac{2}{q} a(u_q, u_q) \quad (31)$$

Proof. Expressions (28) and (29) are obtained by multiplying the differential equation of (6) by u_q and 1 respectively, by integrating on Ω and by using Green's formula. Expression (30) is deduced from (21), (28) and (29). Expression (31) is obtained by deriving (30) with respect to q and by using (26).

Property 8

For all $q > 0$, we have the following expressions

$$(i) f'(q) = k_2 b \text{meas}(\Gamma_2) - \frac{1}{q} a(u_q, u_q) \quad (32)$$

$$(ii) f''(q) = -\frac{1}{q^2} a(u_q, u_q) < 0 \quad (33)$$

Proof. Expression (32) is deduced from (26), (28) and (29), and expression (33) is obtained by using (31) and by deriving (32) with respect to q .

Property 9

There exists a constant $C > 0$ such that

$$a(u_q, u_q) = C q^2 \quad (34)$$

Proof. Let the real function be

$$Y(q) = \frac{1}{q} a(u_q, u_q) \quad (35)$$

defined for $q > 0$. Function Y satisfies the following Cauchy problem:

$$\begin{aligned}
 Y'(q) &= -f''(q) = \frac{1}{q^2} a(u_q, u_q) = \frac{1}{q} Y(q) \\
 Y(0^+) &= \lim_{q \rightarrow 0} 2 \left[k_2 b \text{meas}(\Gamma_2) - \int_{\Gamma_2} u_q d\gamma \right] = 0
 \end{aligned} \quad (36)$$

The solution of (36) is given by

$$Y(q) = Cq \quad \text{with } C > 0 \text{ (constant)} \quad (37)$$

and therefore we obtain (34).

Remark 4

Constant $C > 0$ has the following physical dimension

$$[C] = (\text{cm})^n \quad (38)$$

where n is the dimension of the space \mathbb{R}^n in question.

From (30) y Property 9, it follows:

Corollary 10

Function f , defined by (21), is given by

$$f(q) = -\frac{C}{2} q^2 + k_2 b \text{ meas}(\Gamma_2) q \quad (39)$$

Theorem 11

For all $q > q_1$ problem (7) is a two-phase one, where

$$q_1 = \frac{k_2 b}{C} \text{ meas}(\Gamma_2) \quad (40)$$

Proof. Since $f'(q_1) = 0$, the result follows from (12) and (26).

Property 12

In the case where, because of symmetry, we find that function u_q is constant on Γ_2 , the sufficient condition, given by Theorem 11, is also necessary for problem (7) to be a two-phase one.

Proof. Since $u_q/\Gamma_2 = \text{constant}$, the property follows from the following equivalence

$$\int_{\Gamma_2} u_q d\gamma = 0 \Leftrightarrow u_q/\Gamma_2 = 0 \quad (41)$$

Remark 5

Every thing we proved in this paper is still valid if the boundary Γ of the bounded domain Ω is represented by the union of the three portions ($\Gamma = \Gamma_1 \cup \Gamma_2 \cup \Gamma_3$) such that they have the following characteristics:

- (i) Γ_1 and Γ_2 have the same conditions as the ones previously described in (4).
- (ii) Γ_3 is a wall impermeable to heat, i.e., we have $\partial\theta/\partial n|_{\Gamma_3} = 0$ in (4) and therefore $\partial u/\partial n|_{\Gamma_3} = 0$ in (6).

Remark 6

An analogous problem to the one posed in this paper but for the evolution case has been solved in Ref. 6 for a semi-infinite material which is initially in solid phase, at constant temperature, and which receives a heat flux of the form $-h_0/\sqrt{t}$ ($h_0 > 0$) on its fixed face $x = 0$.

4. NUMERICAL RESULTS

We shall next see the numerical results obtained by using Modulef^{7,8} in two cases for which Property 12 is valid and the solution is explicitly known¹.

Example 1

We consider the following data

$$\begin{aligned} n &= 2, \Omega = (0, x_0) \times (0, y_0) \\ \Gamma_1 &= \{0\} \times [0, y_0], \Gamma_2 = \{x_0\} \times [0, y_0] \\ \Gamma_3 &= [0, x_0] \times \{0\} \cup [0, x_0] \times \{y_0\} \end{aligned} \quad (42)$$

The solution of (6) or (7) is given by

$$u_q(x, y) = k_2 b - qx \quad (43)$$

and then we obtain

$$C = x_0 y_0 \quad q_1 = \frac{k_2 b}{x_0} \quad (44)$$

The numerical results which are below exposed were obtained by doing a simulation process of problem (6) or (7), with the following data:

$$\begin{aligned} x_0 &= 1 \text{ [cm]} \quad y_0 = 1 \text{ [cm]} \quad b = 5 \text{ [}^\circ\text{C]} \\ k_2 &= 0.0014 \left[\frac{\text{cal}}{\text{cm seg } ^\circ\text{C}} \right] \text{ (thermal conductivity of water)} \end{aligned} \quad (45)$$

and by using the following triangulation^{9,10}: 100 2-rectangles of type 1 and 121 vertexes.

$q \left[\frac{\text{cal}}{\text{cm}^2 \text{ seg}} \right]$	$u/\Gamma_2(\text{const}) \left[\frac{\text{cal}}{\text{cm seg}} \right]$
0.0071	-0.0188679
0.00705	-0.00943398
0.007001	-0.000188704
0.00700001	-0.00000191009
0.007	-0.0000000234828
0.0069999998	-0.0000000234828
0.0069999995	-0.0000000234828
0.0069999994	+0.000000627643
0.0069999993	+0.000000627643
0.006999999	+0.000000669955
0.00699999	+0.00000707206
0.0069999	+0.0000713957
0.006999	+0.000714244
0.006998	+0.00142851
0.0699	+0.00714280

We take for q_1 the following approximate value

$$q_{1 \text{ approx.}} = 0.00699999945 \pm 0.00000000005 \quad (46)$$

Since the exact value for q_1 is given by

$$q_{1 \text{ exact}} = 0.007 \quad (47)$$

the error made, by defect, is bounded by

$$0 < q_{1 \text{ exact}} - q_{1 \text{ approx.}} < 6 \cdot 10^{-10} \left[\frac{\text{cal}}{\text{cm}^2 \text{ seg}} \right] \quad (48)$$

Example 2

We consider the following data:

$$n = 2 \quad 0 < r_1 < r_2$$

Ω : annulus of radius r_1 and r_2 , centred in $(0, 0)$

Γ_1 : circumference of radius r_1 and centre $(0, 0)$

Γ_2 : circumference of radius r_2 and centre $(0, 0)$

(49)

The solution of (6) or (7) is given by

$$u_q(x, y) = k_2 b - q r_2 \log \frac{r}{r_1} \quad r = (x^2 + y^2)^{1/2} \quad (50)$$

and then we obtain

$$C = 2\pi r_2^2 \log \frac{r_2}{r_1} \quad \text{meas}(\Gamma_2) = 2\pi r_2$$

$$q_1 = \frac{k_2 b}{r_2 \log \frac{r_2}{r_1}} \quad (51)$$

The numerical results which are exposed below were obtained by doing a simulation process of problems (6) or (7), with the following data:

$$r_1 = 1 \text{ [cm]} \quad r_2 = 2 \text{ [cm]} \quad b = 5 \text{ [}^\circ\text{C]}$$

$$k_2 = 0.0014 \left[\frac{\text{cal}}{\text{cm seg } ^\circ\text{C}} \right] \quad (\text{thermal conductivity of water}) \quad (52)$$

Owing to the symmetry of the problem, it was solved for a quarter of the annulus (the one corresponding to the first quadrant), bearing in mind that in this case a new portion of the boundary Γ_3 appears, which is given by

$$\Gamma_3 = \{0\} \times [1, 2] \cup [1, 2] \times \{0\} \quad (53)$$

Therefore the values for $\text{meas}(\Gamma_2)$ and C are modified in a $1/4$ factor, but the expression of q_1 , which is the value of our interest, does not vary.

We have used in the new domain the following triangulation^{9,10}: 100 2-quadrilateral (two of its sides are segments of lines and the other two are portions of circumferences) of type 1 and 122 vertexes, and we have obtained:

$q \left[\frac{\text{cal}}{\text{cm}^2 \text{ seg}} \right]$	$u/\Gamma_2 \text{ (const)} \left[\frac{\text{cal}}{\text{cm seg}} \right]$
0.004	+ 0.00147440
0.005	+ 0.0000930041
0.00505	+ 0.0000239342
0.00506	+ 0.0000101201
0.0050673	+ 0.00000597593
0.0050674	- 0.000000102207
0.0050675	- 0.000000240374
0.0050677	- 0.000000516654
0.005068	- 0.000000931046
0.00507	- 0.00000369387
0.0051	- 0.0000451358
0.0052	- 0.000183276
0.00535	- 0.000390486
0.0055	- 0.000597696
0.006	- 0.00128840

which gives us for q_1 the following value

$$q_{1 \text{ approx.}} = 0.00506735 \pm 0.00000005 \quad (54)$$

Since the exact value for q_1 is given by

$$q_{1 \text{ exact}} = \frac{0.007}{2 \log 2} \cong 0.00504943 \quad (55)$$

the error made, by excess, is bounded by

$$0 < q_{1 \text{ approx.}} - q_{1 \text{ exact}} < 2 \cdot 10^{-5} \left[\frac{\text{cal}}{\text{cm}^2 \text{ seg}} \right] \quad (56)$$

ACKNOWLEDGEMENT

The present paper has been partly done with the financial support of the GAMNI/INRIA (France). I am also indebted to the fruitful discussions on the use of the Modulef software held with the researchers of the INRIA, in particular with M. Vidrascu.

REFERENCES

- 1 Tarzia, D. A. Sobre el caso estacionario del problema de Stefan a dos fases, *Math. Notae*, 1980/81, **28**, 73-89
- 2 Tarzia, D. A. Aplicación de métodos variacionales en el caso estacionario del problema de Stefan a dos fases, *Math. Notae*, 1979/80, **27**, 145-156
- 3 Duvaut, G. and Lions, J. L. Les inéquations en mécanique et en physique, Dunod, Paris, 1972
- 4 Kinderlehrer, D. and Stampacchia, G. An introduction to variational inequalities and their applications, Academic Press, New York, 1980
- 5 Tarzia, D. A. Introducción a las inecuaciones variacionales elípticas y sus aplicaciones a problemas de frontera libre, CLAMI No. 5, CONICET, Buenos Aires, 1981
- 6 Tarzia, D. A. An inequality for the coefficient σ of the free boundary $s(t) = 2\sigma\sqrt{t}$ of the Neumann solution for the two-phase Stefan problem, *Quart. Appl. Math.*, 1981/82, **39**, 491-497
- 7 Bernadou, M. (Ed.) Modulef: Un code modulaire d'éléments finis. Cours et Séminaires INRIA, Rocquencourt, 26-30 Novembre, 1984
- 8 George, P. L. Utilisation conversationnelle de Modulef, Publications Modulef No. 108, INRIA, Rocquencourt, Mai 1984
- 9 Ciarlet, P. G. The finite element method for elliptic problems, North-Holland, Amsterdam, 1978
- 10 Glowinski, R., Lions, J. L. and Tremolières, R. Analyse numérique de inéquations variationnelles, *Tome 1, 2*, Dunod, Paris, 1976